Community of Yolo Small Community Flood Risk Reduction Feasibility Study

Appendix B Yolo Geotechnical Assessment

Draft April 2019

Table of Contents

Appendix B	Yolo Geotechnical Assessment	. i
B.1	Introduction	1
	B.1.1 Purpose	1
	B.1.2 Background	1
B.2	Existing Levee Information	5
	B.2.1 Existing Levee Assessment: DWR Non-Urban Levee Evaluation	5
	B.2.2 Levee Construction History	6
	B.2.3 Levee Geometry and Freeboard	6
	B.2.4 Past Levee Performance	6
	B.2.5 Geomorphic Setting	7
	B.2.6 Existing Subsurface Explorations 1	1
B.3	Levee Improvement Conclusions	3
B.4	References	5

Tables

Table B-1. Summary of Existing Subsurface Explorations near the Community of Yolo15

Figures

Figure B-1. Community of Yolo Study Area	. 3
Figure B-2. ULE Geomorphology for Cache Creek near the Community of Yolo	. 9
Figure B-2. Existing Subsurface Explorations near the Community of Yolo	13

Acronyms and Abbreviations

CVFPP	Central Valley Flood Protection Plan
cfs	cubic feet per second
CPT	Cone Penetration Test
DWR	California Department of Water Resources
GAR	Geotechnical Assessment Report
Hchy	late Holocene channel deposits

Appendix B Yolo Geotechnical Assessment

Hfy	late Holocene fan deposits
LM	Levee Mile
NULE	Non-Urban Levee Evaluation
Rdc	Historic distributary channel deposits
Rob	Historic overbank deposits
SPFC	State Plan of Flood Control
ULE	Urban Levee Evaluation
URS	URS Corporation
USACE	United States Army Corps of Engineers
WSE	water surface elevation

B.1 Introduction

B.1.1 Purpose

The purpose of this appendix is to describe the geotechnical assessment for the levee repair structural alternatives identified in the Community of Yolo Small Community Flood Risk Reduction Feasibility Study (Feasibility Study). As discussed in the Feasibility Study, six structural alternatives were initially evaluated and screened down to a final array of three alternatives identified as (1) Restore Left Bank of Cache Creek to United States Army Corps of Engineers (USACE) 1957 Design Profile; (2) Levee Improvements for Left Bank of Cache Creek to Pass 100-year Flow; and (3) Restore Left Bank of Cache Creek to USACE 1957 Design Profile and Levee Improvements to pass 100-year Flow. These structural alternatives focus on repairs and improvements to 2,550 feet (approximately 0.5-mile) of Cache Creek left bank levee adjacent to the community of Yolo. This geotechnical assessment considered the existing conditions of this levee extent. An understanding of the existing levee and foundation conditions is essential to identify conceptual remedial levee improvements and facilitate comparative cost assessment for the final array of structural alternatives considered in this Feasibility Study.

B.1.2 Background

The town of Yolo is located approximately 5 miles northwest of the City of Woodland, California. As shown in Figure 1, the community is situated along County Road 99W and the Union Pacific Railroad, south of County Road 17 and Washington Street, west of Cache Creek and County Road 98, and north of County Road 97B and Interstate 5. The community is protected from high water in Cache Creek by the Cache Creek left bank levee, a State Plan of Flood Control (SPFC) levee. Even though the study area for the Feasibility Study encompasses a large area outside the community of Yolo, the Feasibility Study and therefore this geotechnical evaluation focused primarily on the flood risk reduction efforts for the community of Yolo.



Figure B-1. Community of Yolo Study Area

Appendix B Yolo Geotechnical Assessment

B.2 Existing Levee Information

An important component of comparing structural alternatives considered for flood risk reduction in the Feasibility Study is understanding the improvement needs for the existing levees included in the alternatives. Based on the levee improvements identified, costs can be estimated for comparative assessment of the alternatives. Data collected in existing levee evaluation studies and remediation projects were utilized to evaluate the geotechnical conditions of the existing levees adjacent to the community of Yolo.

B.2.1 Existing Levee Assessment: DWR Non-Urban Levee Evaluation

The California Department of Water Resources (DWR) Non-Urban Levee Evaluation (NULE) project included the levees protecting the community of Yolo. The NULE project was completed in two phases but the Cache Creek left (north) bank levee was only included in NULE Phase 1 which was based on desktop studies and readily available data. No subsurface explorations were completed as a part of the NULE Phase 1 study. Assessment data such as historical reports, site interviews with representatives from local agencies (such as levee maintenance personnel or reclamation district representatives), construction records, levee performance records, and other data provided by relevant agencies was collected and reviewed for the study. Geomorphic studies and topographical surveys were also performed.

The collection of information was used to characterize the existing condition of the non-urban levees in the NULE Geotechnical Assessment Report (GAR). The NULE GAR assessment was performed at a single water surface elevation (WSE). For this area the assessment WSE 1957 design WSE profile. Each segment assessed was assigned a hazard category for four geotechnical failure mechanisms: underseepage, slope stability, through seepage, and erosion. The hazard categories assigned for each of these four failure mechanisms were then evaluated collectively to assign an overall hazard level to each segment.

Phase 1 assessments were discretized based on levee segments (typically, levee maintenance units). The levees protecting the community of Yolo are part of a NULE segment that included 11.7 miles of Cache Creek left bank levee. The NULE GAR assessment found this NULE segment to have a high likelihood of levee failure or need to flood-fight to prevent levee failure at the 1957 design WSE profile for potential vulnerability to underscepage, through seepage, and erosion. The NULE Phase 1 study identified the full 11.7-mile segment length for remediations including, waterside rock slope protection to address erosion and a cutoff wall or seepage-stability combination berm to address underscepage and through seepage. The study also identified approximately 70% of the segment as not providing the required three-feet of freeboard above the 1957 design WSE. In many stretches the levee crest is below the 1957 design WSE.

Since the NULE study assessed a larger segment of the Cache Creek left bank than is the focus of this feasibility study, further assessment was warranted to confirm the existing levee conditions for the levee adjacent to the community of Yolo. The follow sections discuss the levee conditions information available in more detail.

B.2.2 Levee Construction History

The Cache Creek levees upstream of the Cache Creek Settling Basin were originally constructed by USACE in 1943 from the mouth of the Cache Creek Settling Basin to the town of Yolo, providing a flow capacity of 20,000 cubic feet per second (cfs). In 1961, the levees along Cache Creek were enlarged to provide a capacity of 30,000 cfs and extended about 3 miles upstream of the town of Yolo (URS, 2014).

B.2.3 Levee Geometry and Freeboard

Topography is available for the community of Yolo study area from DWR's Central Valley Floodplain Evaluation and Delineation (CVFED) LiDAR collected between October 2008 and February 2009. Based on this CVFED LiDAR, levee heights adjacent to the community of Yolo vary approximately 4.5 to 7.5 feet above the landside levee toe. Higher ground is present along the upstream end of the levee, near the railroad and road embankments that run roughly perpendicular to the levee. The crest width is approximately 11 to 14 feet. The landside levee slopes vary from approximately 2H:1V to 3.6H:1V and the waterside levee slopes vary from approximately 2.4H:1V to 4.3H:1V.

The WSEs considered for the Feasibility Study are the 1957 design WSE profile and 100-year flow WSE. Information on the these WSEs is provided in the Feasibility Study Report.

Comparing the existing levee elevations from CVFED LiDAR to the 1957 design WSE profile, the levees adjacent to the community of Yolo are up to one foot below the 1957 design WSE profile in some locations and short of the required three feet of freeboard by three to four feet throughout the levee extent. Due to these freeboard deficiencies, the levees also do not meet their levee prism requirements as minor tributary for a 12-foot crest width at three feet above the WSE, 3H:1V waterside slopes, and 2H:1V landside slopes.

Comparing the existing levee elevations from CVFED LiDAR to the 100-year flow WSE, the levees adjacent to the community of Yolo are above the 100-year flow WSE but are short of the required three feet of freeboard by approximately 1.5 to 2.8 feet. Due to these freeboard deficiencies, the levees also do not meet their levee prism requirements as minor tributary for a 12-foot crest width at three feet above the WSE, 3H:1V waterside slopes, and 2H:1V landside slopes.

B.2.4 Past Levee Performance

The Cache Creek left bank levee near the community of Yolo has experienced reoccurring erosion, numerous boils, and overtopping during past high-water events. Past performance records indicate that erosion has occurred along both the levee slopes and the channel bank. Cache Creek is considered incised near the community of Yolo with deep and steep waterside slopes. Based on past performance, DWR's Flood System Repair Project (FSRP) identified critical and serious past levee performance problem sites along non-urban SPFC levees. Along the Cache Creek left bank levee, the FSRP identified 4 critical erosion sites, including one less than 0.5 miles east of the Yolo community, at approximately LM 2.56. DWR has since constructed a setback levee to address erosion in this location.

Boils have been observed upstream and downstream of Yolo and records report them on the landside slope of the levee and beyond the levee toe, indicating the occurrence of both underseepage and levee through seepage. In several cases, boils have been documented to have had sand bag rings put around them until the flow from the boil stabilized. Some of the levee through seepage occurrences have been attributed to rodent holes/burrows. The Cache creek levees have also experienced overtopping and near overtopping both upstream and downstream of the community.

B.2.5 Geomorphic Setting

The Cache Creek left bank levee was included in the geomorphologic mapping of the DWR Urban Levee Evaluation (ULE) project's Woodland Study Area. An excerpt of this mapping is shown in Figure B-2. As seen in the figure, the levee adjacent to the community of Yolo and much of the upstream and downstream Cache Creek left bank levee is mapped predominantly over late Holocene fan deposits (Hfy). Hfy deposits are typically coarse-grained in nature, since they are deposited under high energy environments and likely consist of poorly sorted sand, silt, and clay deposited by distributary channels on the alluvial fan. The technical memorandum prepared for the geomorphic assessment states, "fan deposits often exhibit prominent natural levees revealed by the topographic contours that form long, sinuous ridges following distributary fan channels. Relatively coarser sediments are expected to underlie portions of the fan surface between these levees and distributary channels (URS, 2013)." A late Holocene channel deposit (Hchy) is mapped beneath the levee and the community approximately halfway through Yolo and likely to be composed of well sorted sands, trace fine gravel, silt, and lesser clay. A historic distributary channel deposit (Rdc) is also mapped just upstream of Yolo. Approximately 0.2 miles upstream from the edge of the community an area of historical overbank deposits (Rob) are mapped. The Rob deposits likely consist of sand, silt, and clay deposited during high-stage water flow overtopping the channel banks. The location mapped is consistent with a location of reported past overtopping.

B.2 Existing Levee Information



Figure B-2. ULE Geomorphology for Cache Creek near the Community of Yolo

Source: Excerpt from Plate 1 from the Technical Memorandum on Surficial Geologic Map and Geomorphic Assessment, California Department of Water Resources Urban Levees Project, Woodland Stud Area, Yolo County, California presented in the URS Supplemental Geotechnical Data Report, Woodland Study Area (URS, 2013)

Appendix B Yolo Geotechnical Assessment

B.2.6 Existing Subsurface Explorations

Existing subsurface exploration data in the vicinity of the community of Yolo were identified and reviewed from available documents. There are no subsurface exploration explorations along levee directly adjacent to the community of Yolo but available nearby data includes recent DWR explorations for erosion repair sites, explorations from the Caltrans bridge database, as well as a few 1958 explorations from USACE levee improvement work. Figure B-3 shows the approximate locations of all of the explorations identified along the Cache Creek left bank between levee mile (LM) 1.0 and LM 3.3.

Under the Sacramento River Bank Protection Project, DWR has evaluated and repaired 7 identified critical erosion sites along the Cache Creek north bank with small setback levees. The working was been done under a State Emergency Erosion Repair Project and a Cache Creek Levee Setback Project and included sites at the following locations:

- LM 0.8
- LM 1.1
- LM 2.5
- LM 2.8
- LM 3.4
- LM 3.9
- LM 4.2

At each erosion project location subsurface exploration was completed by the DWR Division of Engineering Project Geology section. The explorations from the three sites closest to the community of Yolo, (LM 1.1, LM 2.5, and LM 2.8) were reviewed in detailed. The subsurface explorations at these three sites included borings, Cone Penetration Tests (CPTs), test pits, and small trench excavations. The explorations are shown in Figure B-3 and their subsurface stratigraphy summarized in Table B-1. Table B-1 also includes summary of index test results available.

The Caltrans bridge database included 1950s and 1960s records for the Interstate 5 bridges just upstream of the community of Yolo. Additionally, a set of explorations completed in 2000 by Taber Consultants was included in the database, for County Road 99W bridge, adjacent to the upstream end of the community of Yolo. From these available records, six explorations were identified near or along the east bank of Cache Creek. The explorations are shown in Figure B-3 and their subsurface stratigraphy is summarized in Table B-1.

USACE levee improvement drawings from1960 include 19 borings completed in 1958 along the left and right banks of Cache Creek between the Yolo Bypass and high ground. Borings ranged in depth from 24 to 35 feet drilled from the existing levee crown or waterside or landside areas. Closest to the community of Yolo, four of these 1958 explorations are located approximately between LM 2.8 and LM 3.3. The explorations are shown in Figure B-3 and their subsurface stratigraphy is summarized in Table B-1.



Figure B-2. Existing Subsurface Explorations near the Community of Yolo

Table B-1. Summary of Existing Subsurface Explorations near the Community of Yolo

Locations and subsurface stratigraphy are based on available information. USCS classifications may be interpreted from the available information.

	Approximate	Approximate	Approximate Ground Surface Elevation	Total	Exploration	Approximat	e Depths (ft)						Plastic	Moisure Content	
Exploration ID	Levee Mile	Location	(ft, NAVD88)	Depth (ft)	Туре	Тор	Bottom	Soil Type	% Fines	% Sand	% Gravel	Liquid Limit	Limit	(%)	Notes
						0	20	CL	97 96 89	3 4 11	0 0 0	41 38 37	19 16 16	 	
						20	35	ML	96	4	0	49	17		1
CRS2-1	1.10	Setback Foundation	85	82.5	Boring	35	63.5	CL	84 96 55	16 4 45	0 0 0	38 36 26	20 16 10	 	DWR Erosion Repair Project 2005 Boring
						63.5	73.5	SM	31	69	0	22	3		1
						73.5	82.5	CL	90	10	0	39	22		1
CRTP2-1	1.10	Between original levee and setback levee	84	3.7	Test Pit	0	3.7	CL	57 50 72 95	43 50 28 5	0 0 0	29 25 31 45	12 9 12 22	 11 22	DWR Erosion Repair Project 2005 Test Pit
CRTP2-2	1.13	Between original levee and setback levee	84	4.3	Test Pit	0	4.3	CL to CL-ML	59 52 55 96	41 48 45 4	0 0 0 0	27 26 28 43	9 7 11 21	 12 23	DWR Erosion Repair Project 2005 Test Pit
CRS2-2	1.14	Setback levee Foundation	83	52.5	Boring	0	40	CL	89 98 83 98 96 90	11 2 17 2 4 10		44 46 33 47 41	23 '22 13 26 21	 	DWR Erosion Repair Project 2005 Boring
						40	52.5	СН	85	15	0				1
CRT2-1	1.14	Setback Levee Foundation	82	12.7	Trench	0	12.7	CL to ML	89 91 95 98	11 9 5 2	0 0 0 0	39 42 44 45	19 20 22 23	17 18 	DWR Erosion Repair Project 2005 Trench
CRTP2-3	1.15	Between original levee and setback levee	83	4.5	Test Pit	0	4.5	CL	71 94 97	28 6 3	1 0 0	34 43 42	15 21 21	 19 15	DWR Erosion Repair Project 2005 Test Pit
						0	5.5	CL/ML							
CRS2-3	1.22	Levee Crown	89	52.5	Boring	5.5	52.5	CL	90 89 79 83 96 96 94	10 11 21 17 4 4 6		39 39 36 47 44 41	18 17 17 26 22 23		DWR Erosion Repair Project 2005 Boring

			Approximate Ground Surface			Approximat	e Depths (ft)							Moisure	
	Approximate	Approximate	Elevation	Total	Exploration								Plastic	Content	
Exploration ID	Levee Mile	Location	(ft, NAVD88)	Depth (ft)	Туре	Тор	Bottom	Soil Type	% Fines	% Sand	% Gravel	Liquid Limit	Limit	(%)	Notes
						0	3	CL	86	14	0			23	
									72	28	0			12	
						3	1/	ML-CL	6/ 70	33				14	Caltrans boring prior to May 1966.
D 105	1.04		01 5	4.2	Danina				94	6	0			24	
D-105	1.64	Bridge Abutment	91.5	42	Boring	17	21	CL	91	9	0			22	Source elevation assumed to be NGVD29
						17	21	CL	76	23	1				adjusted to NAVD88
								SM and	88	22	0			18	
						31	42	GP-GM	20	27 42	25 50			2	
						0	13	SM							
						13	34	CL-ML							March 1965 Caltrans Bridge Boring.
						34	39	SP and GP							
B-1	1.64	Waterside Bank	81.0	85	Boring	39	59	CL-ML							Souce elevation assumed to be NGVD29,
						59	65	SM							adjusted to NAVD88
						65	85	SP and GP							1
						0	9	SM							
						9	19	SP							
						19	23	SC							December 1952 Caltrans Bridge Boring.
TH-2A	1.66	Waterside Bank	76.9	45	Boring	23	27	CL							Souce elevation assumed to be NGVD29
						27	34	CL-ML							adjusted to NAVD88
						34	40	ML-CL							
						40	45	ML							
						0	3	GP and SP							- June 1951 Caltrans Bridge Boring. - Start elevation well below landside toe
TH-1	1.67	Waterside Bank	56.0	19	Boring	3	19	CL							thickness. - Souce elevation assumed to be NGVD29, adjusted to NAVD88
						0	22	CL							
						22	32	CL]
						32	37	SC							December 2000 Caltrans Bridge Bering
B-3	1 70	Channel	55.0	153 5	Boring	37	77	SP to GP							Start elevation well below landside toe elevation
	1.70	enumer	55.0	155.5	bornig	77	111	CL							therefore cannot evaluate blanket thickness.
						111	121.5	SP-SC							
						121.5	145.5	CL-ML							
						145.5	153.5	SP							
						0	48	CL to ML							
						48	55.5	SM to SP							
CPT-1	1.71	Bridge Abutment	91.0	80	СРТ	55.5	60	CL to ML							October 2000 Caltrans Bridge CPT.
						60	65.5	SM to SP							
						65.5	77	CL to ML							
						77	80	SM to SP							

			Approximate Ground Surface			Approximat	e Depths (ft)							Moisure	
	Approximate	Approximate	Elevation	Total	Exploration								Plastic	Content	
Exploration ID	Levee Mile	Location	(ft, NAVD88)	Depth (ft)	Туре	Тор	Bottom	Soil Type	% Fines	% Sand	% Gravel	Liquid Limit	Limit	(%)	Notes
						0	6	CL	82	18	0				
						6	10	ML							
						10	15	SC	44	56	0	26	8		
						15	17	CL	51	49	0	28	8		
						17	19.5	GP							
CRS3-1	2.41	Levee Crown	83	51.5	Boring	19.5	24.5	SM	25	75	0				DWR Erosion Repair Project 2005 Boring
						24.5	35	CI	86	14	0				
									57	43	0	25	9		4
									00 Q3	7					
						35	51.5	СН	91	9	0				
									85	15	0				
						0	15	CI	80	20	0	38	19		
							1.5		67	33	0	31	13	9	-
						1.5	3.3	SM-SC and CL	 0 /						
00700 4		Between original				33	7.8	MI							
CRIP3-1	2.46	levee and setback	/4	11.5	Test Pit	7.8	9.3	SP							DWR Erosion Repair Project 2005 Test Pit
		levee				9.3	10.2	MI							1
						10.2	10.7	GP and SP							
						10.7	11.5	ML							-
						0	1.8	CL	78	22	0	36	17		
						1.8	3.5	ML							
						3.5	6.2	CL	84	16	0	34	13		1
CRT3-1	2 47	Setback Levee	74	13.8	Trench	6.2	7.6	SM	18	82	0		NP		DWR Frosion Repair Project 2005 Trench
	2.17	Foundation		15.6	in chiefi	7.6	8.1	GP	2	42	55		NP		
						8.1	11.8	SM/SC to	69	30	1	30	11	15	
						11.0	12.0	CL	01	10	-				4
						11.8	13.8	LL	81	19	0	38	18	15	
						0	1.9	CL	74 83	17	0	39	10	12	
		Between original				1.9	7.5	CL to ML	92	8	0	38	16	12	
CRTP3-2	2.48	levee and setback	74	10	Test Pit	7.5	7.9	SM							DWR Erosion Repair Project 2005 Test Pit
		levee				7.9	8.3	ML							
						8.3	9	GP and SP							1
						9	10	SM							1
						0	2	CL							
		Cathoold and				2	8	ML-CL]
CRTP3-5	2.49	Selback Levee	74	12.5	Test Pit	8	9	SP-SM							DWR Erosion Repair Project 2005 Test Pit
		roundation				9	11.8	ML]
						11.8	12.5	CL							

			Approximate			Approximat	e Depths (ft)	-																											
	Approximate	Approximate	Elevation	Total	Exploration								Plastic																						
Exploration ID	Levee Mile	Location	(ft, NAVD88)	Depth (ft)	Туре	Тор	Bottom	Soil Type	% Fines	% Sand	% Gravel	Liquid Limit	Limit																						
									67	33	0	34	16																						
						0	20	CL	84	16	0	34	13																						
									91	9	0	36	13																						
						20	25	СН	95	5	0	60	35																						
		Between original							89	11	0	43	23																						
CRS3-2	2.50	levee and setback	82	60	Boring	Boring 25	44.5	CL	92	8		43	23																						
		levee							97 70	21		51 42	31																						
						44.5	50	sc	12	57	31	4 <u>2</u> 30	16																						
						50	55	SP-SM	6	67	27	20	1																						
						55	60		7	65	27	20	2																						
							00	300-3101	85	15	23	21	2																						
						0	5	CI	62	38	0																								
		Between original				_	_		88	12	0																								
CRTP3-3	2.50	levee and setback	77	11	Test Pit	5	9	ML																											
		levee				9	10.5	SP																											
						10.5	11	GP																											
						0	2.6	CI	82	18	0	35	15																						
					0	2.6		85	15	0	37	16																							
		Between original		10 F	-	2.6	3.5	SM and ML																											
CRTP3-4	2.53	levee and setback	//	12.5	l lest Pit	3.5	10	SM to CL	77	23	0	33	13																						
		levee				10	11	SP																											
						11	12.5	GP																											
						0	5.5	CL	69	31	0	31	15																						
						5.5	13	CL	77	23	0	34	15																						
CRS3-3	2 56	Levee Crown	77	50	Boring	13	20	SC-SM	42	58	0	28	7																						
	2.50		,,,	50	bonnig	20	41	CL	72	28	0	34	17																						
						20	41		95	5	0	48	28																						
						41	50	CL/GC	58	26	16	34	14																						
						0	6	ML																											
						6	17.5	CL	55	45	0	29	12																						
							1,10		60	40	0	30	12																						
	0.50			60		17.5	20.5	SW																											
DH-2.8L-1	2.76	Levee Crown	77	60	Boring	20.5	10		88	12	0	39	17																						
																												20.5	49		95	5		48	26
						10	50	50	15	20	12	39	21 o																						
						49 F2	52		12	/3		21	0																						
						52	60	GP																											

Moisure Content (%)	Notes
	DWR Erosion Repair Project 2005 Boring
	, , , ,
	DWR Erosion Repair Project 2005 Test Pit
/	
	DWR Erosion Repair Project 2005 Test Pit
9	
	DWR Erosion Repair Project 2005 Boring
	Gravel increasing a bottom of boring, last 8.5 feet
	not sampled.
	DWR Erosion Repair Project 2010 Boring

			Approximate			Approximat	e Depths (ft)								
	Annrovimate	Annrovimate	Ground Surface	Total	Evoloration								Plastic	Content	
Exploration ID	Levee Mile	Location	(ft, NAVD88)	Depth (ft)		Тор	Bottom	Soil Type	% Fines	% Sand	% Gravel	Liguid Limit	Limit	(%)	Notes
			(- 71 -	0	3	ML	72	28	0		NP	8	1958 USACE exploration
						3	7.5	SM	50	50	0		NP	12	1
									63	37	0			17	Ground surface elevation based on log elevation
						75	22	NAL	53	47	0			12	and datum conversions. Higher than current
2F-8-4	2.84	Levee Crown	83.3	30	Boring	7.5	22	IVIL	96	4	0			35	ground surface, assumed to be due to
					_		25		79	21	0	4.1	10	29	settlement.
						22	25		80	20	0	41	18	28	-
						25	27.5	IVIL	65 05	35	0		12	19	Souce elevation assumed to be NGVD29.
						27.5	30	CL	85 85	15		36	12	20	adjusted to NAVD88
									53	47	0	27	9	27	
						0	10 E	CI	50	50	0	26	9		
						0	12.5	CL	57	43	0	28	11		
									58	42	0	29	11		-
		Between original				12.5	13	SP							-
DH-2.8L-2	2.85	levee and setback	70	61	Boring	13.5	51	CL to CH	88 03	12		43	21		DWR Erosion Repair Project 2010 Boring
		levee				13.5	51		86	14	0	36	20 15		
						51	54.4	SC							1
						54.4	57	SP-SM	9	70	21		NP		
						57	61	GP							
						0	13	SM to ML							
		Between original				13	43.5	CL to ML							
CP1-2.8L-1	2.85	levee and setback	/0	60	СРТ	43.5	58.5	SP							DWR Erosion Repair Project 2010 CPT
		levee				58.5	60	CL to ML							1
						0	1	CL	71	29	0	31	12	10	
						1	3.5	SC	49	51	0	26	8	6	1
		Between original				3.5	5	SM	20	80	0		NP	4	1
T-2.8L-1	2.85	levee and setback	76	14.5	Trench	5	9	CL	56	44	0	28	10	7	DWR Erosion Repair Project 2010 Trench
		levee				9	9.75	GP-GM							1
						9.75	1/1 5	CI	89	11	0	36	14	28	1
						5.75	14.5	CL	66	34	0	31	12	17	
						0	3	CL to ML							-
		Setback Levee				3	3.5	SP							DWR Erosion Repair Project 2011 CPT
CPT-2.8L-5	2.85	Foundation	69	30.3	СРТ	3.5	14	CL to ML							Elevation estimated from 2008/2009 CVFED
						14	14.5	SP							
						14.5	30.3	CL to ML							
		Setback Levee				0	2	CL to ML							DWR Erosion Repair Project 2011 CPT
CPT-2.8L-4	2.85	Landside Toe	69	30.3	СРТ	2	2.5	SP							Elevation estimated from 2008/2009 CVFED
						2.5	30.3	CL to ML							LIDAR

Exploration iD Levee Wile Location (it, NAVD88) Depth (it) Type Top Bottom Sol Type % Fines % Gravel Equida Linit Linit (%) Notes	
2F-8-5 2.87 Levee Crown 82.5 30 Boring 0 8 ML 61 39 0 NP 18 0 8 13 SM 41 59 0 NP 11	
2F-8-5 2.87 Levee Crown 82.5 30 Boring 8 13 SM 41 59 0 NP 11 0 2F-8-5 2.87 Levee Crown 82.5 30 Boring 0 10 10 11 23 Ground surface elevation based on log and datum conversions. Higher than cu	
2F-8-52.87Levee Crown82.530Boring76240311123Ground surface elevation based on log and datum conversions. Higher than cu	
21-6-5 2.87 Level Crowit 82.5 50 Borning 96 4 0 55 11 55 and datum conversions. Higher than cu	25.05
	25-0-2
13 30 CL 51 15 20 ground surface, assumed to be due to	
90 10 0 37 13 28 settlement.	
90 10 0 44 20 26	
65 35 0 18 1958 USACE exploration	
2F-8-6 2.88 Levee Crown 82.9 30 Boring 30 Boring 32 and datum conversions Ligher than a	2F-8-6
90 10 0 35 groupd surface, assumed to be due to	
68 32 0 18 settlement.	
28 30 CL 90 10 0 36 15 28	
Between original 0 49.5 CL to ML	
CPT-2.8L-2 2.91 levee and setback 70 60 CPT 49.5 58 SP DWR Erosion Repair Project 2010 CPT	CPT-2.8L-2
levee 58 60 CL to ML	
0 6 CL	
6 8 GP	
8 13 SC 37 40 23 30 11	
DU 2 81 2 2 3 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2	
DH-2.8L-3 2.93 Levee Crown 76 60 Boring 19.3 20.2 SC DWR Erosion Repair Project 2010 Boring	DH-2.8L-3
20.2 60 CL to CH 92 8 0 40 16	
<u> </u>	
0 7 SP 5 95 0 NP 3	
7 8 SM 18 82 0 NP 8	
8 10.5 SP 5 95 0 NP 3 Ground surface elevation based on log	
2F-8-7 3.27 Waterside 75.4 27.5 Boring 35 65 0 9 and datum conversions. Higher than cut	2F-8-7
10.5 24 SM 44 56 0 All NP 10 ground surface, assumed to be due to	
18 58 24 12 24 265 SP 4 62 34 26 10 4	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	

As shown in Figure B-3, the available explorations generally fall into five areas, the explorations in each of these areas are discussed further below.

Upstream of the community of Yolo there are seven 2005 subsurface explorations available from DWR's State Emergency Erosion Repair Project site at LM 1.1. The explorations included three borings which were completed to depths of approximately 50 to 80 feet, three test pits from 3.7 to 5.5 feet deep, and a small trench excavation to 12.7 feet deep. One of the borings went through the levee crown and logged the embankment as containing clay and silt. All of the explorations found the foundation to be predominately composed of clay and silt materials. The deepest boring encountered a 10-foot thick silty sand layer beginning at a depth of 63.5 feet below the landside ground surface.

Near LM 1.7, slightly upstream of the community of Yolo, there are six bridge relate subsurface explorations. The explorations included 5 borings and one CPT and range in depth from 19 feet to 153.5 feet. A mix of fine-grained (silt and clay) and coarse-grained (sand and gravel) material was encountered in all of the explorations. Two of the borings identified a sandy shallow foundation with no fine-grained blanket at the surface. The sandy material in these borings went to depths of up to 23 feet below the ground surface. Where present, the fined-grained blanket appeared to be approximately 24 to 41 feet thick. Records reviewed did not include information on bridge abutment construction and if any treatment or improvement was made to the embankment or shallow foundation in these locations that would create different subsurface conditions at these locations than elsewhere along the nearby Cache Creek left bank levee. The two borings that identified a sandy shallow subsurface were from 1951 and 1952, prior to the Interstate 5 construction in 1956.

Downstream from community of Yolo there are nine 2005 subsurface explorations available from DWR's State Emergency Erosion Repair Project site at LM 2.5. The explorations included three borings which were completed to depths of 50 to 60 feet, five test pits to 10 to 12.5 feet deep, and a small trench excavation to 13.8 feet deep. Two of the borings went through the levee crown and identified the embankment to be composed of lean clay. A fine-grained blanket was identified in foundation all of the explorations. In most locations, the blanket thickness ranged from approximately 7 feet to 14 feet thick, but in one location the blanket thickness was up to approximately 44 feet thick. Zones of sand and often gravel were encountered below the blanket in all explorations that extended past the bottom of the blanket layer. The deepest exploration terminated in sand at 60 feet below the landside ground surface.

Further downstream of the community of Yolo there are eight 2010 and 2011 subsurface explorations available from DWR's Cache Creek Levee Setback Project site at LM 2.8. Additionally, in this area there are three 1958 USACE explorations. In total, the 11 explorations in this area included 6 borings and 4 CPTs to depths of approximately 30 to 60 feet and one small trench excavation to 14.5 feet deep. Two of the explorations encountered coarse-grained materials (sand and/or gravel) in the shallow foundation, with no fine-grained blanket above them. One of the CPT also identified a potentially sandy surface layer. The thickness of the surficial sands ranged from 5 feet to 13 feet. Two other CPTs identified likely sandy lenses in the upper 5 feet of the blanket. The remaining explorations generally identified a fine-grained blanket approximately 11 feet up to almost 50 feet thick. Two of the deeper borings, encountered

Appendix B Yolo Geotechnical Assessment

sand underlain by gravels at the bottom of the explorations, as deep as about 60 feet below the ground surface.

The last exploration, one of the 1958 USACE explorations, is further downstream at approximately LM 3.27. This exploration encountered surficial sands to a depth of 26.5 feet. The boring terminated at 27.5 feet and encountered clay in its final foot.

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B.3 Levee Improvement Conclusions

The goal of this geotechnical assessment was to identify conceptual remedial levee improvements for the levee adjacent to the community of Yolo to facilitate the costs assessment for the final array of structural alternatives considered in the Feasibility Study. Considerations included potential repairs for erosion, freeboard, and underseepage, through seepage, and landside slope stability.

Performance history indicates erosion has been a consistent problem along this stretch of levee and repair is recommended. To address erosion the Feasibility Study will consider placement of rock slope protection along the waterside of the levee and the channel bank slope.

As summarized in Section B.2.3, freeboard repairs are needed for both the 1957 design WSE profile and the 100-year flow WSE. To meet 1957 design WSE profile freeboard requirements, the levees adjacent to the community of Yolo would need to be raised approximately 0 to 4 feet. To meet 100-year flow WSE profile freeboard requirements, the levees adjacent to the community of Yolo would need to be raised approximately 0 to 2.8 feet. Freeboard repairs would also address levee prism (geometry) requirements.

Review of underseepage, through seepage, and stability remediation needs were based on available subsurface information and the past performance of the levees near the community of Yolo. Past performance of the levees near Yolo includes records of through and underseepage There were not records of past landside slope instability in the area. Explorations through the levee generally found a fine-grained levee embankment composed of clay and silt. Animal burrows are suspected to be contributing to the past through seepage problems. Available explorations identified generally variable foundation conditions. Surficial sand layers up to 26.5 feet thick provide concern for shallow underseepage. There is also concern for deeper underseepage, with locations of thin fine-grained blankets and deeper sand and gravel units. The bottom depth of some of the encountered pervious zones is not known based on the available exploration information as some borings, up to 60 feet deep, ended in sand or gravels. Therefore, to address underseepage and through seepage, a cutoff wall is recommended. A cutoff wall is the most practical remedy for this project site as there is not adequate space at the landside levee toe for a seepage berm solution. Based on the unknown depth of the underlying aquifer, a cutoff wall to a depth of 80 feet (the limit of conventional open trench wall construction) will be assumed for this Feasibility Study.

B.4 References

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